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CCE4242-Robotics

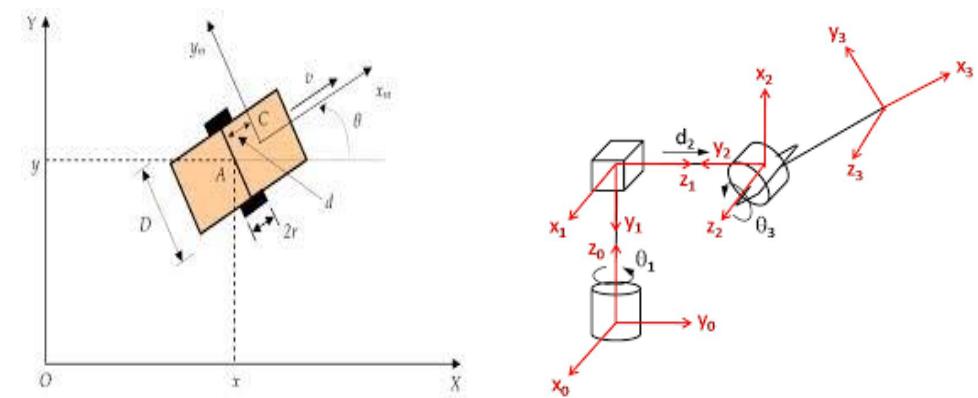
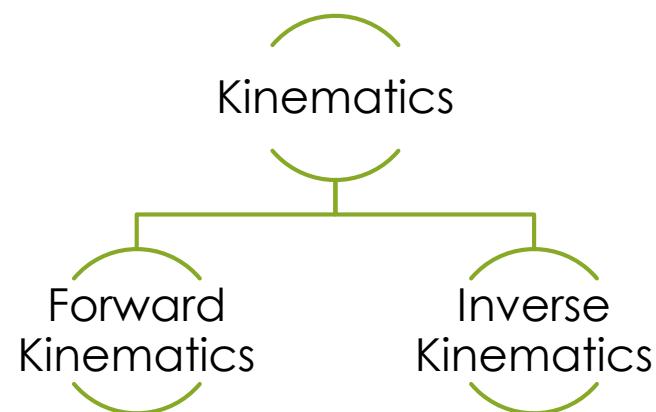


# Robot Forward Kinematics

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# Introduction

- ▶ Robot kinematics:
  - ▶ Description of motion of the robot without consideration of the forces and torques causing the motion.
  - ▶ The Kinematics is a geometric description.



# Forward and Inverse Kinematics

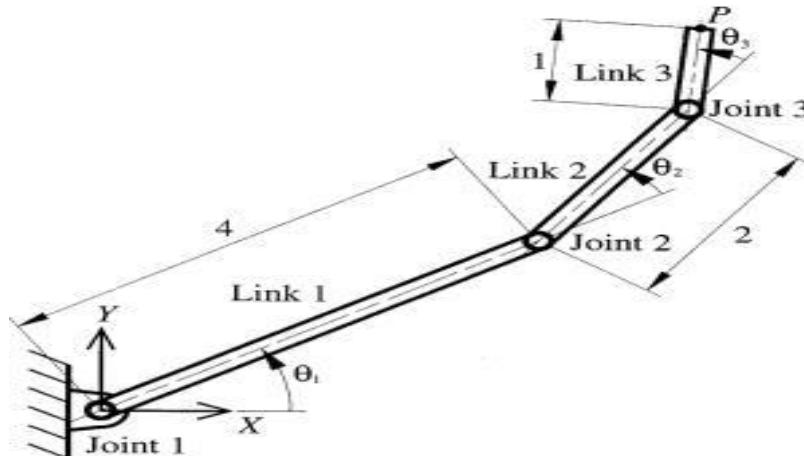
- ▶ Forward Kinematics
  - ▶ Determination of the (actual) position and orientation of the end-effector given the values for the joint variables of the robot
- ▶ Inverse Kinematics
  - ▶ Determination of the values of the joint variables of the robot given the (desired) position and orientation of the end-effector
- ▶ Notes
  - ▶ Inverse Kinematics is required to determine the control action
  - ▶ Forward kinematics is required to give feedback about end-effector pose

# Kinematic Chains

MANIPULATORS  
FORWARD KINEMATICS

# Robot Manipulators

- ▶ A robot manipulator is composed of a set of links connected together by joints.
- ▶ A robot manipulator with  $n$  joints will have  $n + 1$  links as each joint connects two links.



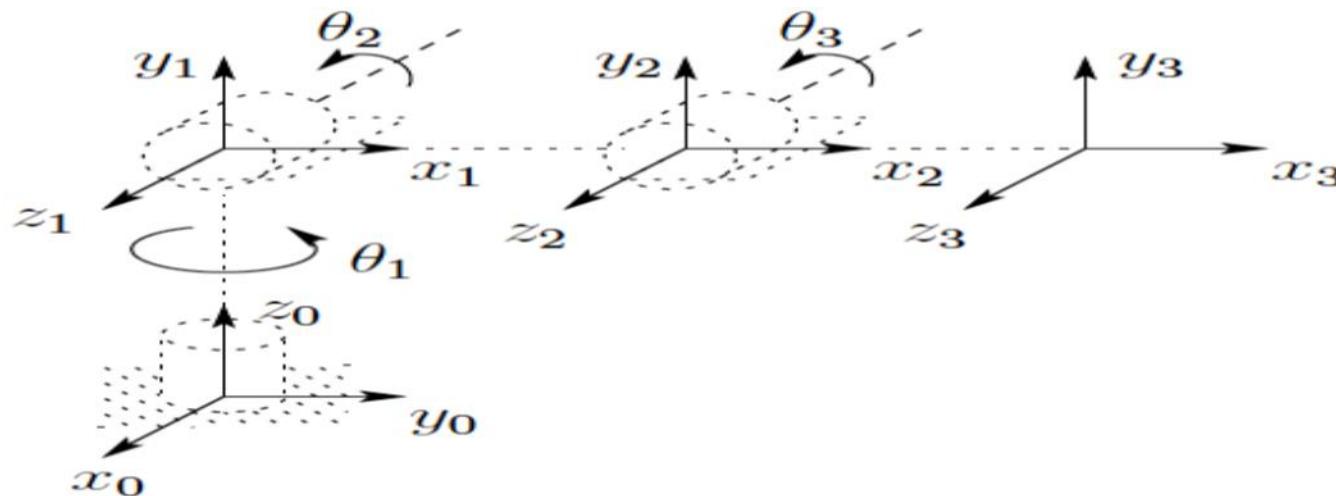
# Robot Manipulators

## ► Convention

- We number the joints from 1 to  $n$  , and we number the links from 0 to  $n$  , starting from the base.
- By this convention, joint  $i$  connects link  $i - 1$  to link  $i$ . We will consider the location of joint  $i$  to be fixed with respect to link  $i - 1$ .
- When joint  $i$  is actuated, link  $i$  moves.
- With  $i^{th}$  joint we associate a joint variable, denoted by  $q_i$ 
  - Angle of rotation in case of revolute joint
  - Joint displacement in case of prismatic joint

# Kinematics Analysis

- ▶ To perform the kinematic analysis, we attach a coordinate frame rigidly to each link. In particular, we attach frame  $o_i x_i y_i z_i$  to link  $i$ .
- ▶ The frame  $o_0 x_0 y_0 z_0$ , which is attached to the robot base, is referred to as the inertial frame.



# Kinematic Analysis

- ▶ Suppose  $A_i$  is the homogeneous transformation matrix that expresses the position and orientation of  $o_i x_i y_i z_i$  with respect to  $o_{i-1} x_{i-1} y_{i-1} z_{i-1}$ .
- ▶  $A_i$  is a function of only a single joint variable, namely  $q_i$ .
  - ▶  $A_i = A_i(q_i)$
- ▶ The homogeneous transformation matrix that expresses the position and orientation of frame  $o_j x_j y_j z_j$  with respect to frame  $o_i x_i y_i z_i$  is denoted by:

$$T_j^i = \begin{cases} A_{i+1} A_{i+2} \dots A_{j-1} A_j & \text{if } i < j \\ I & \text{if } i = j \\ (T_i^j)^{-1} & \text{if } j < i \end{cases}$$

# End-Effector Pose

- ▶ The position and orientation of the end-effector with respect to the inertial frame are denoted by a vector  $O_n^0$  (represents the coordinates of the origin of the end-effector frame with respect to the base frame) and a rotation matrix  $R_n^0$  respectively.
- ▶ The homogeneous transformation matrix of end-effector pose  $H$  is:

$$H = \begin{bmatrix} R_n^0 & O_n^0 \\ 0 & 1 \end{bmatrix}$$

$$H = T_n^0 = A_1(q_1) \dots \dots A_n(q_n), \quad A_i = \begin{bmatrix} R_i^{i-1} & O_i^{i-1} \\ 0 & 1 \end{bmatrix}$$

# Pose components

- ▶ For homogeneous transformation matrix  $T_j^i$

$$T_j^i = A_{i+1} A_{i+2} \dots \dots A_j = \begin{bmatrix} R_j^i & O_j^i \\ 0 & 1 \end{bmatrix}, \quad j > i$$

$$R_j^i = R_{i+1}^i R_{i+2}^{i+1} \dots \dots R_j^{j-1}$$

$$O_j^i = O_{j-1}^i + R_{j-1}^i O_j^{j-1}$$

# Review Example

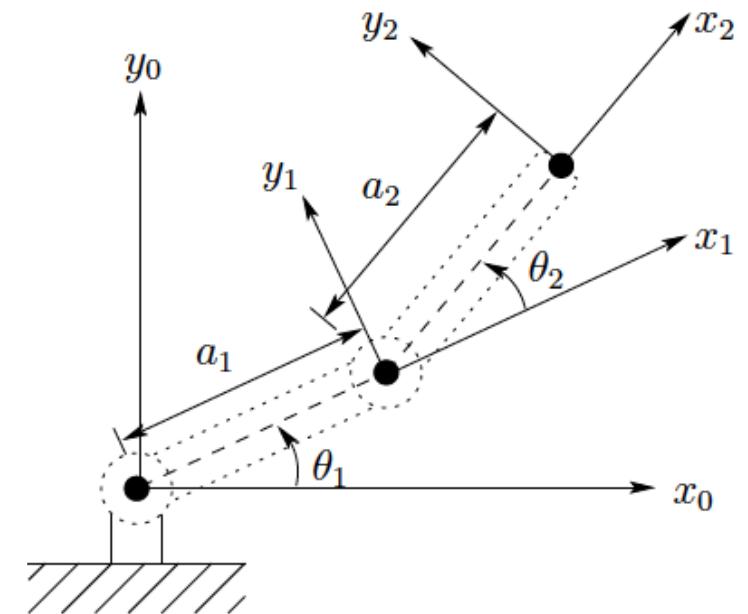
- Consider the two-link planer manipulator

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1 c_1 \\ s_1 & c_1 & 0 & a_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad T_1^0 = A_1$$

$$A_2 = \begin{bmatrix} c_2 & -s_2 & 0 & a_2 c_2 \\ s_2 & c_2 & 0 & a_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad T_2^0 = A_1 A_2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1 c_1 + a_2 c_{12} \\ s_{12} & c_{12} & 0 & a_1 s_1 + a_2 s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Note:  $c_1 \equiv \cos(\theta_1)$ ,  $c_{12} \equiv \cos(\theta_1 + \theta_2)$

$s_1 \equiv \sin(\theta_1)$ ,  $s_{12} \equiv \sin(\theta_1 + \theta_2)$



# DH-Convention

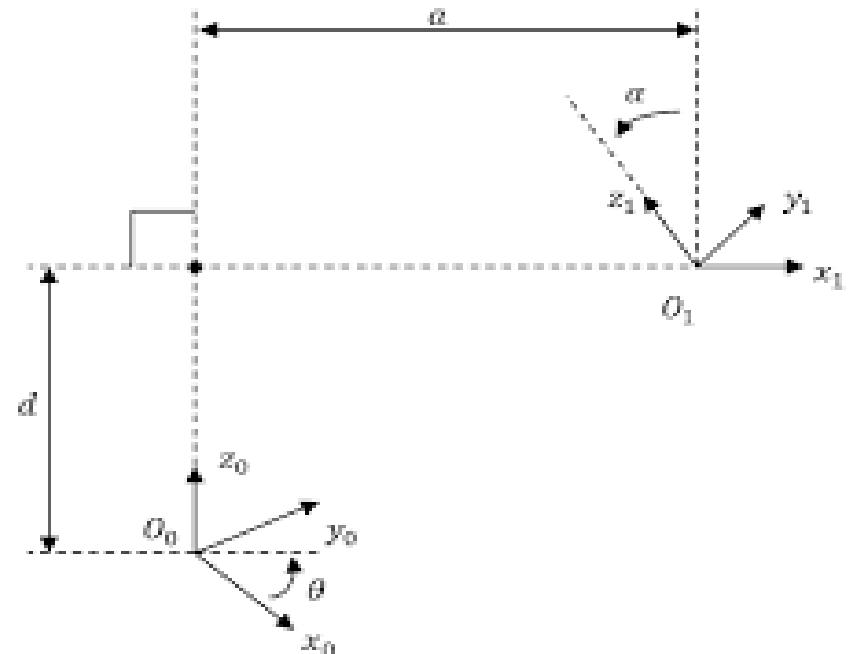
DH ASSUMPTIONS  
ASSIGNING FRAMES

# Denavit-Hartenberg convention

- ▶ Denavit-Hartenberg convention or DH convention is a commonly used method for selecting reference frames of robots
- ▶ In DH convention, the 6 parameters associated with an arbitrary homogeneous transformation are reduced to 4 by appropriate selection of reference frames
- ▶ In this convention, each homogeneous transformation  $A_i$  is represented as a product of four basic transformations using the following parameters:
  - ▶  $a_i$ : Link length
  - ▶  $\alpha_i$ : Link twist
  - ▶  $d_i$ : Link offset
  - ▶  $\theta_i$ : joint angle

# DH-Assumptions

- ▶ DH coordinate frame assumptions
  - ▶ DH1- The axis  $x_i$  is perpendicular to the axis  $z_{i-1}$
  - ▶ DH2- The axis  $x_i$  intersects the axis  $z_{i-1}$
- ▶ Under the above assumptions  $A_i$  is achieved by
  1.  $Rot(z, \theta_i)$
  2.  $Trans(z, d_i)$
  3.  $Trans(x, a_i)$
  4.  $Rot(x, \alpha_i)$
- ▶  $A_i = Rot(z, \theta_i) * Trans(z, d_i) * Trans(x, a_i) * Rot(x, \alpha_i)$



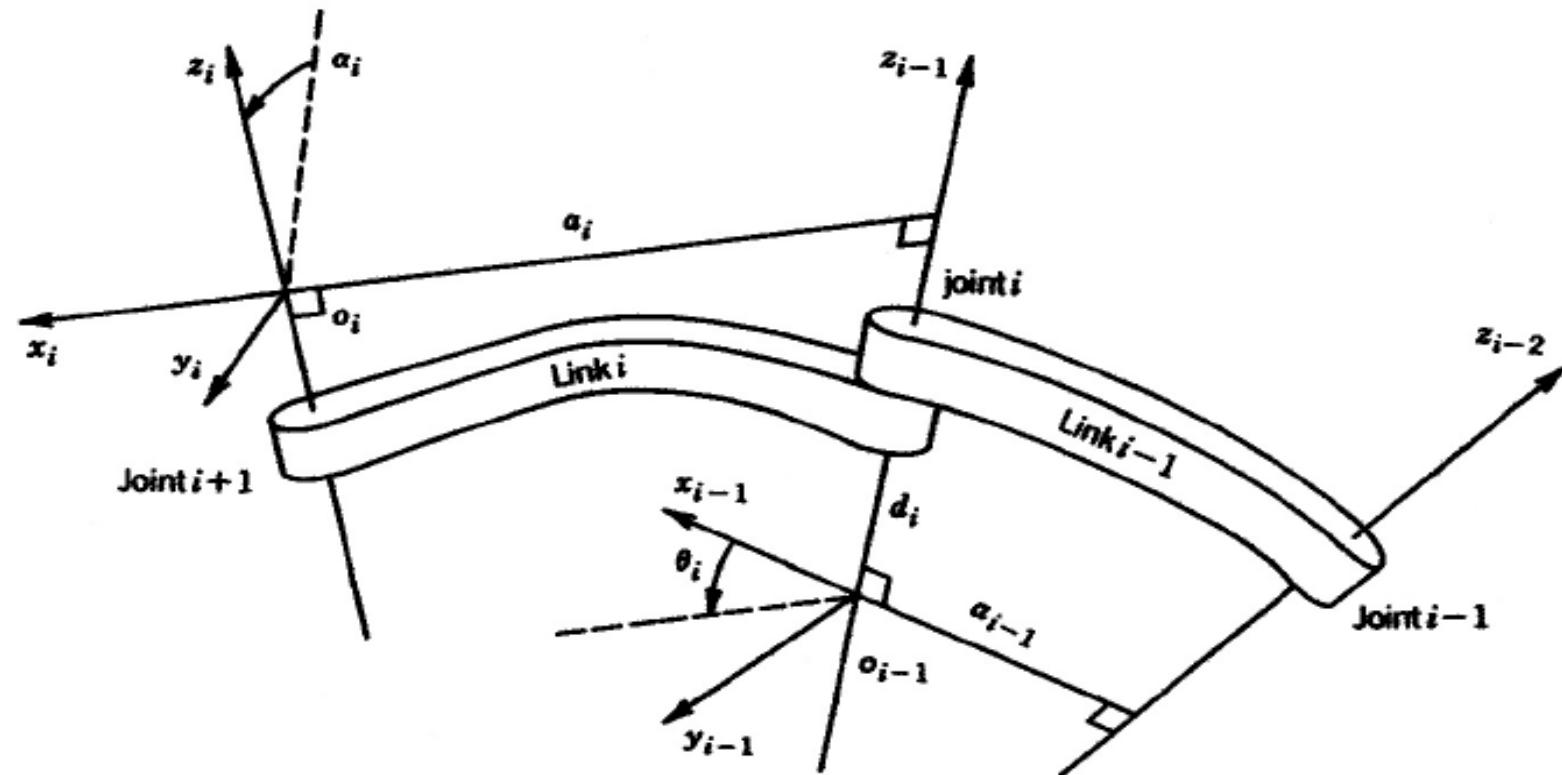
# DH-Assumptions

$$\begin{aligned}
 A_i &= Rot_{z,\theta_i} Trans_{z,d_i} Trans_{x,a_i} Rot_{x,\alpha_i} \\
 &= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i} & 0 & 0 \\ s_{\theta_i} & c_{\theta_i} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
 &\quad \times \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & c_{\alpha_i} & -s_{\alpha_i} & 0 \\ 0 & s_{\alpha_i} & c_{\alpha_i} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
 &= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i}c_{\alpha_i} & s_{\theta_i}s_{\alpha_i} & a_i c_{\theta_i} \\ s_{\theta_i} & c_{\theta_i}c_{\alpha_i} & -c_{\theta_i}s_{\alpha_i} & a_i s_{\theta_i} \\ 0 & s_{\alpha_i} & c_{\alpha_i} & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}
 \end{aligned}$$

# DH-Parameters

- ▶ The parameter  $a$  is the distance between the axes  $z_0$  and  $z_1$  measured along the axis  $x_1$
- ▶ The parameter  $\alpha$  is the angle between the axes  $z_0$  and  $z_1$ , measured in a plane normal to  $x_1$  axis
- ▶ The parameter  $d$  is the perpendicular distance from the origin  $O_0$  to the intersection of the  $x_1$  axis with  $z_0$  axis measured along the  $z_0$  axis
- ▶ The parameter  $\theta$  is the angle between  $x_0$  axis and  $x_1$  axis measured in a plane normal to  $z_0$  axis
- ▶ Hint:
  - ▶  $d$ : is, only, the variable in case of prismatic joints
  - ▶  $\theta$ : is, only, the variable in case of revolute joints

# Coordinate Frames Assignment



# Assignment steps

1. Assign  $z_i$  to be axis of actuation of joint  $i + 1$
2. Establish arbitrarily the base frame:  $x_0, y_0, (z_0$  determined in step 1)
3. Define  $x_i$  based on one of three cases
  - a. The axes  $z_{i-1}$  and  $z_i$  intersect
  - b. The axes  $z_{i-1}$  and  $z_i$  are parallel
  - c. The axes  $z_{i-1}$  and  $z_i$  are not coplanar
4. Define  $y_i$  in the appropriate direction to complete the frame
5. The final coordinate frame  $o_n x_n y_n z_n$  is commonly referred to as the end-effector or tool frame. The origin  $O_n$  is most often placed symmetrically between the fingers of the gripper

# Assignment of $x_i$ axis

## $z_{i-1}$ and $z_i$ are intersected

- $x_i$  is chosen normal to the plane formed by  $z_{i-1}$  and  $z_i$  .
- The positive direction of  $x_i$  is arbitrary.
- The most natural choice of  $o_i$  to be at the intersection point of  $z_{i-1}$  and  $z_i$
- In this case  $a_i$  equal zero

## $z_{i-1}$ and $z_i$ are parallel

- There are infinitely common normal between them
- DH1 doesn't specify  $x_i$  completely
- It's free to choose  $o_i$  anywhere along  $z_i$
- The normal going through  $o_i$  is chosen to be  $x_i$

## $z_{i-1}$ and $z_i$ not coplanar

- There exists a unique shortest line segment from  $z_{i-1}$  to  $z_i$ , perpendicular to both of them
- This line segment defines  $x_i$
- The point where the line of  $x_i$  intersects  $z_i$  is the origin  $o_i$

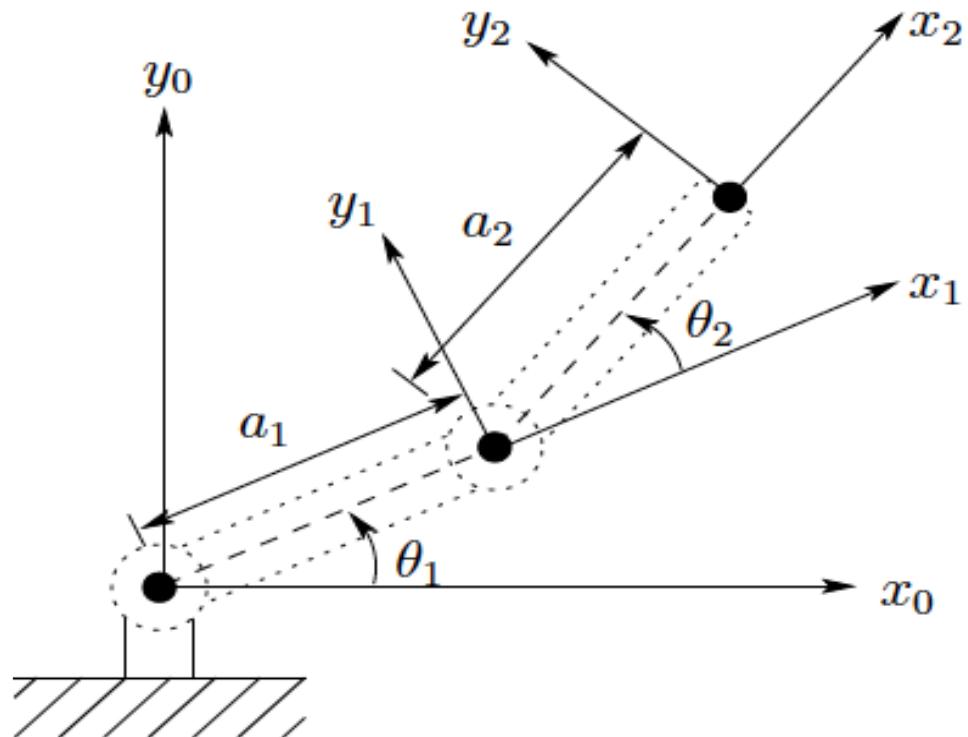
# Examples

PLANAR MANIPULATOR  
CYLINDRICAL ROBOT

# DH-solution steps

- ▶ Assignment of coordinate frames according to the defined rules
- ▶ Construction of DH-Table containing the parameters of each transformation matrix between two successive links
- ▶ Compute the transformation matrix  $A_i$  for each link
- ▶ Compute the whole homogenous transformation matrix  $T_n^0$
- ▶ Remember:
  - ▶  $A_i = Rot(z, \theta_i) * Trans(z, d_i) * Trans(x, a_i) * Rot(x, \alpha_i)$
  - ▶  $H = T_n^0 = A_1(q_1) \dots \dots A_n(q_n)$

# Two-Link Planar Manipulator



Link parameters for 2-link planar manipulator

Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1^*$
2	$a_2$	0	0	$\theta_2^*$

\* variable

# Two-Link Planar Manipulator

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1 c_1 \\ s_1 & c_1 & 0 & a_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

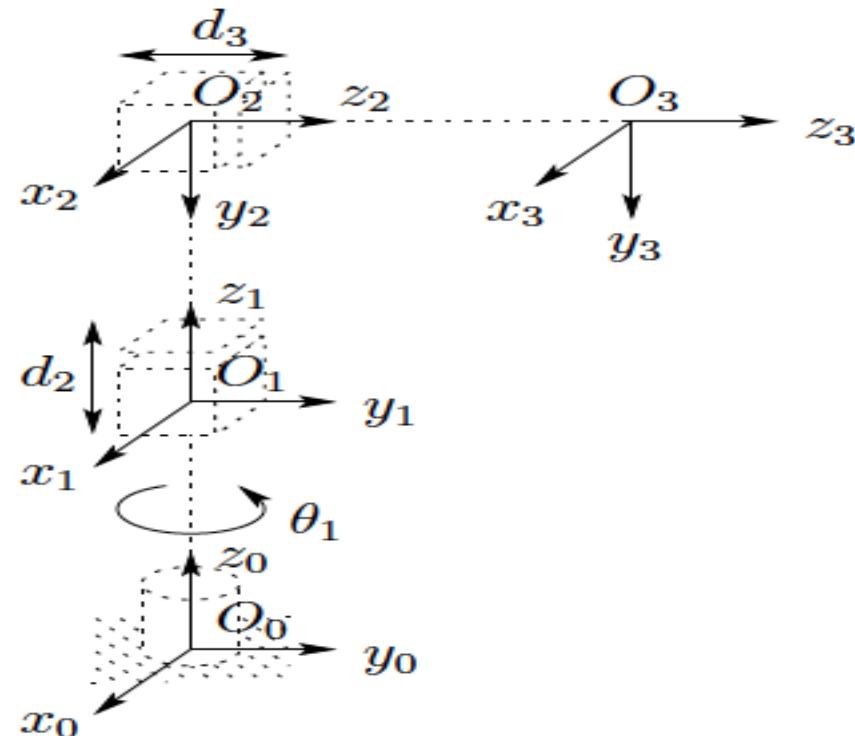
$$A_2 = \begin{bmatrix} c_2 & -s_2 & 0 & a_2 c_2 \\ s_2 & c_2 & 0 & a_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

The  $T$ -matrices are thus given by

$$T_1^0 = A_1$$

$$T_2^0 = A_1 A_2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1 c_1 + a_2 c_{12} \\ s_{12} & c_{12} & 0 & a_1 s_1 + a_2 s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Three-Link Cylindrical Robot



Link parameters for 3-link cylindrical manipulator

Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	0	$d_1$	$\theta_1^*$
2	0	-90	$d_2^*$	0
3	0	0	$d_3^*$	0

\* variable

# Three-Link Cylindrical Robot

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_3^0 = A_1 A_2 A_3 = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Reference

- ▶ Mark W. Spong, Seth Hutchinson and M. Vidyasagar,  
“Robot Modelling and Control”, Wiley, 2005

